In-Situ Comparison of Water Supply Well Gravel Packs

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- Overview of SJW's McLaughlin Station Project
- Comparison of different gravel pack materials
 - \circ Design
 - o Constructability
 - o Development
 - \circ Performance
 - o Cost
- Project challenges



SJWC – McLaughlin Station



- Four+ acre site
- Room for multiple wells
- Existing homes
- Recreation field



Test Hole-Monitoring Well

- Small diameter test hole
- Sample collection
- Geophysical surveys
- Installation of multiple piezometers
- Sieve analysis
- Collection & analysis of water samples
- Long term water level monitoring





U.S. Standard Sieve Numbers

Cumulative Percent Retained

Slot Opening and Grain Size in Thousandths of an Inch



Slot Opening and Grain Size in Thousandths of an Inch

McLaughlin Production Well

- 1,800 GPM
- Deep annular seal
- 18" Diameter
 - 0.3125" Copper bearing blank
 - $\,\circ\,$ 0.3125" and 0.375" Stainless steel blank
 - $\,\circ\,$ 0.3125", 0.055" Louvered well screen
- Gravel fill and sounding pipes
- 8x16 Cemex (Monterey) gravel



McLaughlin Station Layout

- Six production wells
- Test hole/monitoring well
- Minimum spacing 150'
- All wells constructed by same contractor
- Wells constructed and tested
 between March 2016 & April 2017



Gravel Pack Materials



Premier Silica

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- Texas
- Rounded, spherical sand
- Uniform shape
- 99% Silica
- Chemical resistant
- Standard gradations and blends
- NSF certified



Premier Silica 6x9



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- Monterey, CA
- Rounded sub rounded
- Spherical to lenticular
- 91% Silica
- Chemical resistant
- Standard gradations and blends
- NSF certified
- Works well in fine sands



CEMEX 6x12

Sili (Sigmund Linder) Beads

Spherical glass beads Uniform size, shape No stratification Consistent, optimal packing Smooth Resistant to compression Soda Lime Glass Chemical resistant

Shorter development times Higher yields, specific capacity Longer rehabilitation intervals, more effective

Sili 4508R 0.0787"-0.0945"



U.S. Standard Sieve Numbers

Slot Opening and Grain Size in Thousandths of an Inch

U.S. Standard Sieve Numbers

Slot Opening and Grain Size in Thousandths of an Inch

Production Well Elogs

- Test hole 45' from Well No. 5
- Upper zones consistent
 across site
- Formation depths/thickness diverged with depth
- Wells were redesigned in field

w/0.055" Slot Size

w/0.055" Slot Size

w/0.055" Slot Size

w/0.070" Slot Size

| Well | Slot Size (in) | Pack Material | Screen Open Ended (ft) (hrs) | | Swab/Airlift (min/ft) | Pump Development (hrs) | |
|------|-------------------|------------------|---------------------------------|-----|--------------------------|------------------------------|--|
| 1 | 0.070 | 6x12 C | 167 | 3.8 | 14.4 | 40.0 | |
| 2 | 0.070 | 4508R | 165 | 2.5 | 13.9 | 38.3 | |
| 3 | 0.055 | 4507R | 135 | 6.0 | 18.2 | 41.0 | |
| 4 | 0.055 | 8x16 C | 167 | 3.0 | 18.0 | 50.0 | |
| 5 | 0.055 | 8x16 P | 167 | 3.8 | 14.6 | 40.5 | |
| 6 | 0.070 | 6x9 P | 166 | 4.5 | 13.4 | 37.0 | |
| | | Averag | ge Times | 3.9 | 15.4 | 41.1 | |

- Average swab/airlift development for larger slot/gravel designs: 13.9 min/ft
- Average swab/airlift development for smaller slot/gravel designs: 16.9 min/ft
- Time savings of 8.3 hours

San Jose Water Company McLaughlin Wells 8-hour Constant Rate Tests

Pump Testing

| Well | Slot Size (in) | Pack Material | Screen (ft) | Flow Rate (gpm) | Specific Capacity (24 hr, gpm/ft) |
|------|-------------------|------------------|----------------|--------------------|---|
| 1 | 0.070 | 6x12 C | 167 | 1,831 | 75 |
| 4 | 0.055 | 8x16 C | 167 | 1,773 | 62 |
| 5 | 0.055 | 8x16 P | 167 | 1,773 | 48 |
| 2 | 0.070 | 4508R | 165 | 1,806 | 46 |
| 6 | 0.070 | 6x9 P | 166 | 1,848 | 33 |
| 3 | 0.055 | 4507R | 135 | 1,808 | 32 |

| cu | | | | | | | | | | | | | 100 |
|-----------|----------|---------------|-----------------------------|------------|----------|-------|----------------|-------------------------|-------------|-----------|--------|-------|----------|
| | STOM | ER: | | | | | | - | - | | | | |
| Pur | ping W | ell: #1 | Test Type: | 8 HR | Step Tes | it. | Constant I | tatë 🖌 | Recovery | 1 118 | Monite | iring | _ |
| Loca | tion: n | in Lough | A test Oper | itor: D | ARYL | Whi | HLEY | | | | | _ | |
| SW2- | 59 | 45 | Oate/Time | 8. | 15:14 | | | Pumping | Rate (GP | ME 190 | 0 | | |
| 1.2000 | uring Pi | aint- | Test Startin | ng Date/Ti | mes | ×. | 25-16 | 81 | 00 A | m | | | |
| 10042 | ining Pr | tine stanille | VCC Tait Endla | Date/Tis | hua : | | | | | | | | - |
| Meas | uring PC | MILL CARY AV | Contraction and Contraction | 100107-10 | 04 | | 1001000 | | TTAK. | 1 12 | | | |
| Pump | Depth: | - | Duration: | - | STAL | | 140433 | No. of Concession, Name | LE IVI. | | | - | 1 |
| Degred To | a Tine | or latence La | at Totalizer | WTU: | COM. | Stod | Elapsed Time | Time or | Weter Lawer | Totalizer | NTU | GPM | Sand |
| (Min) | Fm Re | ndiel(855) | - | - | | - | 110 | - Aller | 8210 | 19063 | 1.12 | 1804 | TRACE |
| nos. | - | - | - | | | | 120 (2 HIRS) | | 83,21 | 190670 | 1. Per | 1802 | |
| - | - | 40.3 | 3 190459 | | 1806 | | 1/2 150 HR | 10:30 | \$3.28 | 190725 | 1.27 | 1792 | |
| | 1 | 167 2 | 5 190461 | | 1815 | | 180 (3 885) | 11:00 | 83.94 | 190779 | 1.03 | 1804 | TRACE |
| - | 1 | 81.00 | 190413 | | 1827 | | 210 | 11:30 | 84.15 | 190832 | 0,94 | 1812 | TRACE |
| 6 | 1 | 41.2 | 21190465 | - | 0.000 | 2 | 240 (4HRS) | 12:00 | 33.60 | 190887 | 0.98 | 1803 | |
| 7 | | 81.4 | 190467 | | 1814 | | 300 (S HIRS) | 12:30 | 82.48 | 190941 | 1.14 | 1869 | LENCE |
| | | \$1.53 | 190468 | | 1514 | 1 | 340 (E HIRS) | 1:00 | 31.89 | 190995 | 10.68 | 1813 | |
| | | 51.55 | 190470 | | 1812 | | 420 (7 HRS) | 1:30 | 31.18 | 191049 | 0.88 | 1819 | - |
| 10 | | 81.68 | - 1904 72 | | 1797 | | 480 (8HR5) | 2:00 | 30.8 | 191103 | 0.67 | 1819 | 1 |
| 12 | | 81.80 | 190477 | | 1806 | | 540 (9 HRS) | 2:30 | 80.3 | 191158 | 0,82 | 1804 | TRIEF |
| 34 | | \$1.83 | 190480 | 3.62 | 1804 | TREEF | 600 (10 HRS) | 3:00 | 30.19 | 191212 | 110 | 1813 | |
| 16 | | 51,99 | 190483 | | 1804 | | 660 (11 HRS) | 3:30 | 79.83 | 191260 | 0.90 | 1807 | TRACE |
| 18 | | 81.97 | 190487 | | 1801 | | ,720 (12 HRS) | 4:00 | 179.70 | | 0.70 | 180 | Trace |
| 10 | | 82.0 | 190490 | Z.10 | 1804 | TEACE | 780 (13 HRS) | | | | | | 9 10 10 |
| 5 | | 82-12 | 190501 | | 1807 | | 840.(14 HRS) | | | | | | |
| 0 | | 82.15 | 190509 | 2.22 | 1802 | | 900 (15 HRS) | | | | | | |
| s | | \$2,20 | 190518 | | 1780 | TEARE | 960 (16 HRS) | | | | | | 1 |
| | | 82.41 | 190526 | 1.74 | 1797 | - | 1020 (17 HRS) | | | | | | |
| | | \$2.75 | 190536 | | 1805 | | 1080 (18 HRS) | | | | | | 100 |
| | | 82.78 | 190545 | 1.81 | 1810 | | 1140 (19 HRS) | | 1 | | | 100 | 1000 |
| | . 0 | 87.88 | 190554 | | 1802 | Teres | 1200 (20 HRS) | | | | | | 1. |
| ini la | - | 82.81 | 19057.3 | | IVAC | 1 | 12/01210051 | | | | | | |
| | | 87.60 | 190581 | 1.07 | ICN | | 1320 [22 March | | | | | - | depost - |
| - | - | 21.87 | 190094 | 101 | 1001 | - | ASAD (22 HRS) | | - | - | - | | 12-13-14 |
| - | | 03.0 | 100/8 | 0.01 | 1811 | Ten - | 1380 (23 HRS) | - | - | | 1 | | - |
| - | | 03.0 1 | 10010 | 0.36 | 1866 | TRACE | 1440 (24 HRS) | - | - | | - | 10 | - |
| | 8 | 3.08 1 | 90635 | | 1801 | | | 1 | - | | - | 10 | |

Sili Beads Vs Traditional Gravels

- Must handle Sili Bead bags carefully
- No observed time savings during gravel packing operations
- Sili Beads bagged in smaller bags than gravel
 potential lost time
- Uniformity of Sili Beads means no stratification in bags or annulus
- Consistent packing (Optimal?)
- No clear advantage during development
- Not readily available long lead time
- Cost \$\$\$

Pack Material Costs

| Material | Cost Per Ton ¹ | Cost for McLaughlin Well ² | Additional Cost for Sili | | |
|--------------------------------|---------------------------|--|-----------------------------|--|--|
| Sili 450708 (0.066"-0.098") | \$1,406 | \$108,262 | | | |
| Premier 6x9 | \$390 | \$30,030 | \$78,232 | | |
| Premier 8x16 | \$362 | \$27,874 | \$80,388 | | |
| Cemex 6x12 | \$242 | \$18,643 | \$91,616 | | |
| Cemex 8x16 | \$197 | \$15,169 | \$93,093 | | |

¹ – List Price, ² – 77 tons

Beads are 3.5-7x more than gravels

Conclusions

- Not an ideal comparison of gravel pack performance due to:
 - Changes in lithology across site
 - Inconsistent well designs
 - Water level variations throughout project
- No one pack material stood out as clearly superior in regards to constructability or development
- Monterey sands had highest specific capacity
- Sili Beads are 3.5 to 7 times the cost of other pack materials
- Supply/distribution infrastructure for Sili Beads not adequate

- Testing of all wells once equipped to define baseline performance values
- Develop standardized well performance testing protocol and schedule
- Long term program to collect and analyze well performance data
- Track cost, effort, frequency, and effectiveness of well rehabilitations

Acknowledgements

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